DEMONSTRATION AND EVALUATION OF THE AIR FORCE SITE CHARACTERIZATION AND ANALYSIS PENETROMETER SYSTEM IN SUPPORT OF NATURAL ATTENUATION INITIATIVES VOLUME III - DEMONSTRATION, TESTING, AND EVALUATION AT PATRICK AFB

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PREFACE

This report was prepared by Applied Research Associates, Inc. (ARA), 120-A Waterman Road, South Royalton, VT 05068 under U. S. Air Force Contract No. F08635-93-C-0020, SSG Subtask 8.01.1 for the Armstrong Laboratory Environics Directorate, AL/EQW-OL, 139 Barnes Dr. Suite 2, Building 1120, Tyndall AFB, FL 32403-5323.

This final report discusses the continued development of the combined technology of the cone penetrometer (CPT) and laser-induced fluorescence (LIF) as it pertains to the detection and quantification of petroleum oils and lubricants (POL's) within subsurface soils environments. Specifically the report covers a review of LIF-CPT technology; LIF-CPT system specifications; evaluation of the LIF-CPT probe under field conditions; and LIF data analysis/evaluation. The data and results of the field investigations were subsequently used to determine if bioventing or natural attenuation approaches are viable remedial alternatives at three U.S. Air Force Bases.

The work was performed between October 1993 and December 1994. The AL/EQW project officer was Mr. Bruce Nielsen.

EXECUTIVE SUMMARY

A. OBJECTIVE

Applied Research Inc. (ARA) and Dakota Technology, Inc. (DTI) were retained by the Armstrong Environics Directorate AL/EQ-QL to further develop laser-induced fluorescence-cone penetrometer technique (LIF-CPT) for use during environmental site investigations. The primary objective of the program was to develop and evaluate an improved LIF-CPT system for the characterization of fuel-contaminated sites. The evaluation was based on the results from demonstrations, testing and evaluation at three Air Force bases. A parallel goal of the demonstrations was to gather data for Engineering-Science, Inc. (E-S) to determine if bioventing or natural attenuation are viable alternatives for remediating numerous Air Force sites.

B. BACKGROUND

The Department of Defense (DoD) is seeking efficient and cost effective means to assess, remediate, and monitor petroleum-contaminated and hazardous waste sites at both active and decommissioned installations. The Air Force's Installation Restoration Program Information Management System (IRPIMS) database lists approximately 1,400 fuel-contaminated sites and 300 inactive firefighter training facilities; presently the IRPIMS database contains data from only one-half of the installations. Current environmental site investigations based on drilling technology are slow, expensive and potentially dangerous. Cone penetrometer (CPT) based investigations, on the other hand, allow real-time data collection and don't produce soil cuttings thus eliminating disposal costs and health and safety risks due to exposure.

Cone penetrometer testing gathers accurate in situ geotechnical information in a rapid and cost-effective manner. With adaptation of in situ geophysical and chemical sensors to the cone penetrometer probe, subsurface hydrogeology and the extent of contamination can be mapped simultaneously. The speed and continuous nature of the information generated by LIF-CPT reduces the need for costly and invasive subsurface sampling and installation of long term monitoring wells.

C. SCOPE

To fulfill the objectives of this project, the following tasks were completed; (1) Development, fabrication and integration of a field-deployable, wavelength-tunable LIF system, (2) Laboratory testing and evaluation of the LIF system, (3) Demonstration, testing and evaluation programs at Plattsburgh, Patrick/Cape Canaveral, and Dover Air Force Bases (AFB's), and (5) Delivery of a completed LIF system to the U. S. Army Corp. of Engineers.

Extensive evaluation and calibration of the LIF-CPT remained outside of the scope of this project. Such a study could not be completed during this project due to the dual objectives of

developing the LIF-CPT, and employing the tool and other CPT capabilities on a production basis for the engineering-cost evaluation conducted by E-S.

D. METHODOLOGY

The United State Army Corp of Engineers Waterways Experimental Station (USAE WES) initially developed the LIF-CPT using a mercury lamp as an excitation source downhole within the cone. The resulting fluorescence was collected and directed to a detection system located in the cone penetrometer truck via a single optical fiber. WES soon eliminated the mercury lamp in favor of a pulsed laser source external to the cone; a nitrogen laser system, limited to the emission of a single excitation wavelength of 337 nanometer (nm) was employed. This was useful for the detection of large multi-ring fuels such as Diesel Fuel Marine (DFM) but proved ineffective for "lighter" fuels such as jet fuels and gasoline which require excitation at shorter wavelength. Further research sponsored by the Air Force concluded that a tunable wavelength, pulsed laser (Nd:YAG) with a fiber optic probe and detection system would satisfy the needs of the Air Force. During the scope of the current program Applied Research Associates, Inc., in cooperation with Dakota Technology, Inc. (DTI), refined the Nd:YAG pulsed LIF-CPT system and demonstrated its utility in the field.

E. TEST DESCRIPTION

The test program consisted of two phases; (1) redesign and build a new laser system based on the findings of a previous LIF-CPT development program, and (2) evaluation of the LIF-CPT system under field conditions at three Air Force Bases. The redesign of the LIF-CPT system consisted of two major efforts: (1) optimizing the overall laser system performance by upgrading individual components with state-of-art components and repackaging the system improving portability and durability, (2) redesign the LIF-CPT probe to maximize the performance and durability and minimize cost. During the field demonstration and evaluation program several objectives were addressed. The primary technical focus was to evaluate the LIF-CPT system in the field for reliability, stability and repeatability, correlation of LIF-CPT intensity to contaminate concentration and evaluation of the sources of data scatter in the chemical and LIF-CPT data.

F. RESULTS

During the three demonstrations the laser system performed quite well. Many of the system improvements greatly enhanced both field utility and system stability. Minor improvements are still needed to enhance power stability, although the recording of the current power levels is highly beneficial.

Evaluation of the LIF response shows that there are effects related to both the soil type and moisture content of the materials being tested. The effect of soil type is fairly significant, since at some locations no LIF response was recorded in visibly contaminated clay samples. The effect of

moisture content is minimal. Further investigation into these responses would be highly beneficial. Finally, the limited data sets available permitted only speculation about possible correlations between LIF response and to be performed. The results form the statistical analysis are encouraging and additional testing performed.

G. CONCLUSIONS

In general the LIF and chemical analytical data agree well qualitatively. Evaluation of the limited chemical and LIF data indicates that their may be a correlation between total BTEX and Xylene concentrations and LIF response. The background limit of the LIF response was determined to be independent of the soil type but may have a weak dependency on moisture content. The background limit of the current LIF-CPT probe configuration is approximately 50 counts. There are still some unanswered questions regarding the response of the LIF system in different soils. Areas known to be highly contaminated showed little or no response in fine grained soils (e.g., silts and clays). Insufficient chemical data was available to fully validate the LIF system.

H. RECOMMENDATIONS

Additional data collection and evaluation is required to fully validate the LIF-CPT system. For future testing, it is strongly recommended that on-site analytical screening for Total Petroleum Hydrocarbons (TPH) by EPA method 418.1 be conducted on soil samples. This data can subsequently be used to correlate TPH concentration to LIF response. Combining objectives that include production-oriented data collection for other research is not recommended.

I. APPLICATION

The LIF-CPT system can be implemented by the Air Force as the primary technology to conduct environmental site assessments where petroleum, oils and lubricants are the contaminants of interest. It could be used both as an initial screening tool and/or as a tool to monitor the effectiveness of a particular remedial effort.

J. BENEFITS

Significant reductions in the time and cost of conducting environmental site assessments could be realized by implementing the LIF-CPT technology. This system provides superior data in real-time to use as a basis for selecting an appropriate remedial strategy.

K. TRANSFERABILITY OF TECHNOLOGY

Virtually all industrial contractors involved with subsurface environmental site assessments where petroleum oils and lubricants are concerned could profit from the use of LIF-CPT technology. The industry in general is constantly seeking ways to conduct business faster, cheaper, and better; CPT-LIF fulfills these criteria.

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SECTION I INTRODUCTION

A. OBJECTIVE

The Armstrong Laboratory Environics Directorate (AL/EQ-OL) retained Applied Research Associates, Inc. (ARA) to demonstrate, test, and evaluate (DT&E) the application of the Air Force Site Characterization and Analysis Penetrometer System (AFSCAPS) in support of the Air Force's intrinsic remediation (natural attenuation) initiatives. One of the key components of the AFSCAPS involves the use of a Nd:YAG dye pumped laser system to induce fluorescence as the CPT probe is advanced into the soils. Laser-Induced Fluorescence (LIF) has been shown to be useful in identifying Petroleum, Oil, and Lubricant (POL) contamination.

ARA and their subcontractor, Dakota Technologies, Inc. (DTI), in cooperation with Engineering-Science, Inc. (E-S), the United States Environmental Protection Agency (USEPA) Robert S. Kerr Environmental Research Laboratory (RSKERL), and the CES/CEV office at Patrick Air Force Base conducted an intensive subsurface investigation of soil and groundwater at the ST-29 site located at Patrick Air Force Base (AFB), Florida, and the former fire training area at Kennedy Space Center, Cape Canaveral, Florida. This investigation commenced 21 March 1994 and was completed on 01 April 1994. The three objectives of this investigation were to:

- Demonstrate the CPT's capabilities to quickly locate and define the areal and vertical
 extent of the liquid-phase plume using LIF, and to rapidly install monitoring points and
 collect soil samples to provide additional data necessary to define the dissolved-phase
 plume, and
- Adequately assess the subsurface conditions at the ST-29 site to allow E-S to model the potential for natural attenuation using the Bio-Plume II numerical model,
- Provide data collection capabilities to support the United States Environmental Protection Agency's (EPA) efforts aimed at modeling the fate and transport of chlorinated solvents at the former fire training area noted above.

This data report contains a brief description of the site, data obtained and a brief interpretation of the data.

B. BACKGROUND

Historically, the cone penetrometer has been employed as an expeditious and effective means of analyzing the lithology of a site by measuring the resistance of different soil types against the penetrometer probe as it is advanced into the subsurface. ARA has expanded the CPT's capabilities in several ways to allow further definition of the subsurface environment.

The DTI Nd:YAG laser system was integrated into the CPT by ARA and DTI to locate fuel contamination using the LIF response of the soil/fuel mixture. Subsequently, the LIF response can be correlated to the total petroleum hydrocarbon (TPH) concentration present within the soil. To date, the LIF laser system's primary function has been to define the liquid phase plume.

To aid in defining the dissolved-phase plume, ARA has developed a rapid method of installing small-diameter (0.5-inch) monitoring wells. These wells are typically installed based upon the LIF-CPT data and can be installed to any desired depth with a screened interval typically ranging between 1 to 2 meters. The wells are constructed using 0.5-inch slotted PVC well screen and either 0.5-inch PVC or 0.25-inch OD Teflon® tubing as riser material. Experience has demonstrated that these wells perform well in aquifers where the depth to the potentiometric surface (water table under unconfined conditions) does not exceed the suction capacity of a vacuum pump (typically about 25 feet below grade).

Collection of soil samples serves several purposes. First it provides a physical specimen with which the CPT data can be correlated. In essence, it allows the observer to look at the CPT cone tip and sleeve stresses combined with the pore water pressure data indicated on the CPT logs and compare it directly with the in situ soils. This allows for accurate interpretation of the CPT logs and subsequent interpretation of the overall site lithology. Secondly, subsequent chemical analysis of the soil samples for total petroleum hydrocarbons (TPH) provides a correlation between LIF data and the in situ TPH concentrations. Finally, additional chemical analysis of the soil samples provides data required to both model the natural attenuation potential of the site using the Bioplume II numerical model and develop correlation between the LIF response and the level of soil contamination.

SECTION II SITE DESCRIPTION

The efforts of this investigation were primarily devoted to the ST-29 site (Figure 1, Site Map) located at Patrick AFB. However, a limited investigation was conducted at the former fire training area located at the Kennedy Space Center, Cape Canaveral, Florida. The following sections pertain to the ST-29 site describing the site geology, hydrogeology, and soil and groundwater quality. This information was extracted from the work plan prepared by Engineering-Science, Inc. (Ref. 1) for this site. Only limited background information pertaining to the fire training area was available at this time.

A. SITE GEOLOGY AND HYDROGEOLOGY

Patrick AFB and Kennedy Space Center, Cape Canaveral Air Force Station (AFS) are situated on undifferentiated marine sands and the Pleistocene-age Anastasia and Caloosahatchee Marl Formations; these three units comprise the surficial unconsolidated deposits in the area. The Anastasia Formation is a discontinuous layer of undifferentiated sands with silt and shells. Acting as a semi-continuous confining unit at a depth of approximately 50 feet, the Caloosahatchee Marl Formation consists of calcareous, sandy clay deposits. Above the semiconfining layer, the surficial deposits form a shallow, unconfined aquifer. Underlying the Caloosahatchee Formation is the Tamiami Formation, which is made up of limestones, marls, silty sands, and clay. The Tamiami Formation forms a shallow bedrock aquifer. The marine sands, clays, and limestones of the Hawthorn Formation underlie the Tamiami Formation. Interspersed limestone layers form localized aquifers within the Hawthorn Formation. Beneath the Hawthorn Formation is the Floridan Aquifer, which is comprised of Ocala Limestone and extends to a depth of over 1,500 feet below mean sea level.

The surface geology at Site ST-29 consists of fine- to coarse-grained sand which is poorly to moderately sorted and contains up to 40 percent shell fragments (Ref. 2). The marine sand deposits of the top 25 feet at the site are of Holocene and Pleistocene age. These sand deposits contain interspersed organics with dark gray and black discolorations from petroleum constituents. Soil boring samples exhibited organic vapor readings ranging from background levels to greater than 200 ppmv. The Anastasia Formation is discontinuous in this area and therefore was not found in some areas of Site ST-29. The Caloosahatchee Marl formation was reported to be encountered between the depths of 25 and 51 feet below grade (Ref. 2). This soil layer is blue and

gray in color, with dense, moderately well-sorted, very fine- to medium-grained silty sand with 5 to 65 percent shell fragments. Organic constituents were detected throughout the deposit and were prevalent in distinct thin beds about 0.25 foot thick. No soil discoloration or organic vapor readings above background were noted in these soils. A deposit of clay marl was encountered from 51 feet below grade to at least 57 feet below grade. This layer is typified by blue-gray to dark green soil with shell and limestone fragments, and correlates with the semi-confining, discontinuous layer of sand and silt deposits that occur within the Caloosahatchee Marl.

The shallow groundwater at Site ST-29 resides in an unconfined aquifer at depths of 3.5 to 4.5 feet below grade. The hydraulic gradient at the site ranges from 0.00096 to 0.003 foot per foot (feet/feet) (Ref. 2; Ref. 3). No slug test data are available for the site. An estimated average hydraulic conductivity of 0.26 foot per minute was obtained from data gathered in other areas of Patrick AFB. It was assumed that the soil lithologies throughout Patrick AFB are relatively similar (Ref. 2). Groundwater at the site may be subject to alternating directions of flow toward the Banana River or towards the Atlantic Ocean. This groundwater anomaly is probably related to the operation of locks and dams southwest of the base that are used to control the water levels in the Banana River relative to the Atlantic Ocean. The likelihood of contamination of the deep aquifer from sources in the shallow aquifer is assumed to be minimal because the deep aquifer has sufficient pressure head to cause the potentiometric surface for the deep aquifer to be greater than that for the water table within the shallow unconfined aquifer (Ref. 2).

Patrick AFB receives its water from the City of Cocoa Beach, Florida, which is supplied by in-land well fields screened in the Floridan aquifer in East Orange County, Florida. A backup water supply for Patrick AFB is supplied by the City of Melbourne, Florida. Patrick AFB maintains five standby potable water supply wells primarily for fire suppression use. These wells are screened in Ocala Formation limestones that host the confined Floridan Aquifer (Ref. 4). Groundwater in the surficial aquifer beneath Site ST-29 is classified as G-II based on the FAC

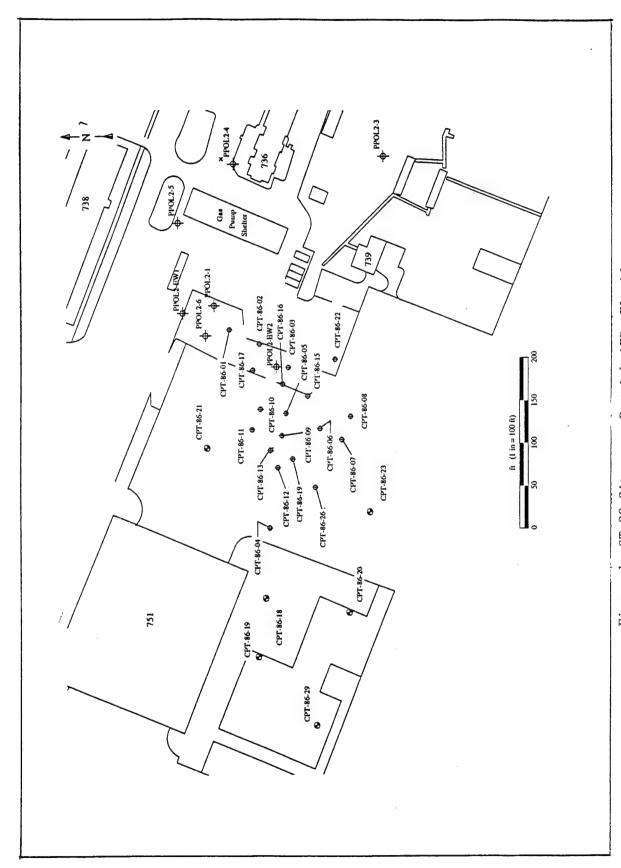


Figure 1. ST-29 Site map, Patrick AFB, Florida.

regulations, Chapter 3 [designated as potable if less than 10,000 milligrams per liter (mg/L) of total dissolved solids is present].

B. SOIL QUALITY

Contaminant sources at Site ST-29 include the five abandoned 5,000-gallon MOGAS USTs northeast of the BX Service Station (Building 736) and the area surrounding the four operational 10,000-gallon MOGAS USTs, situated southeast of the service station. Site characterization data from previous investigations detected organic vapor levels that exceeded 50 ppmv in soil borings SB-1, SB-2, SB-3, SB-5, and SB-6 (SB-1 recorded at 200 ppmv; SB-2 recorded 170 ppmv) (Ref. 5). Organic vapors levels in other samples from the remaining soil borings and from the monitoring well borings were relatively low (2 to 13 ppmv). Most soil samples exhibited peculiar odors described variously by the on-site geologist as petroleum (most samples), alcohol, diesel, old gasoline, sulfur, and organic matter. No soil or groundwater samples were submitted for laboratory analyses during the previous investigation because the site had not been included in the IRP until Stage 2 testing.

The collection and analysis of soil samples from eight boreholes completed during the previous investigations indicated a high level of petroleum hydrocarbons at sample location SB-2 on the west side of the car wash. Xylenes were found in SB-1, SB-2, SB-3, and SB-8, with values ranging from 22.3 milligrams per kilogram (mg/kg) in SB-1 to 822 mg/kg-dry in SB-2. Ethylbenzene and toluene were detected in boreholes SB-2, SB-3, and SB-8, with the high value of ethylbenzene and toluene being 100 mg/kg-dry and 38 mg/kg-dry, respectively, in SB-8. An additional contaminant source of potential concern is an unlocated, abandoned UST located somewhere north and/or east of the existing BX Service Station. An attempt by ESE to locate this tank with an electromagnetic survey was unsuccessful. Based on analysis of samples from a deep well located downgradient of the site, soil and groundwater contamination had not occurred at depth at the time of the study.

None of the data obtained from previous testing can be used to fully characterize the lateral or vertical extent of contamination. The soil borehole reports (Ref. 5) and soil gas studies (Ref. 6) during soil headspace analysis indicate the area of highest identified soil contamination is near the car wash. This suggests that fuel may be migrating from the vicinity of the MOGAS USTs located northeast of the car wash building, or that the area was impacted by a surface fuel spill. A bioventing unit installed in a 20-foot vapor extraction trench along the northeast side of the car wash is currently in operation at the site. During installation of the bioventing unit, soil was

visually saturated with hydrocarbon contamination. Bioventing operations are expected to reduce these soil contamination levels near the car wash.

C. GROUNDWATER QUALITY AND CHEMISTRY

Groundwater was sampled at Site ST-29 during previous site characterizations (Ref. 2). Volatile compounds and chlorinated compounds were detected at low concentration in all six wells. Wells PPOL2-1, PPOL2-2, and PPOL2-4 contained the highest concentration of contaminants. All these wells are located downgradient of either the abandoned USTs northeast of the service station building or downgradient of the operational USTs on the southwest side of the BX service station. Although the contaminant levels detected in groundwater are low, the existing groundwater monitoring wells may not be situated properly to allow detection of all groundwater contamination, especially in the vicinity of the car wash. The extensive soil contamination in the area surrounding the car wash suggests that groundwater contamination may be greater than previously indicated. The soils at the site are highly permeable, unconsolidated sands with shell fragments and minor amounts of clay and organic matter. Therefore, a contaminant plume may be migrating away from the car wash, under the tarmac to the west.

SECTION III RESULTS

During the course of the Patrick AFB investigation, ARA completed 18 LIF-CPT soundings. Figure 1 depicts the locations of these soundings. Based upon this data 40 successful 0.5-inch monitoring wells were installed to various depths to allow collection of groundwater samples for subsequent chemical analyses. In addition, 19 soil samples were obtained to provide additional data required for the Bioplume II modeling and to allow correlation with both the CPT and LIF profiles. A summary of the soundings completed and the respective well completion details and soil sampling intervals at this site is included in Table 1.

Eleven LIF-CPT soundings were completed at the former fire training area located at the Kennedy Space Center, Cape Canaveral. Interpretation of this data allowed effective placement of 11 monitoring wells and collection of eight soil samples. A summary of soundings completed and respective well completion details and soil sampling intervals is included in Table 2.

A. INTERPRETATION OF CPT PROFILES

Inspection of the CPT profiles indicate that the overburden soils at the ST-29 site consist of various gradations of sands with occasional discontinuous seams of silty clays and clay. This interpretation is in good agreement with findings from previous investigations (Ref. 1). The basis for this interpretation is presented below.

Comparison of tip stress, friction ratio and penetration pore pressure profiles are the most important parameters for estimating soil type and stratigraphy from CPT data. The magnitude of the tip resistance is a function of the strength of the soil, with stronger materials having higher tip resistances. Tip resistance also increases as the coarse grained soil content increases, and decreases as the fine grained content increases. The degree of consolidation of the soils can influence tip resistance with both the tip and sleeve stresses increasing as the degree of consolidation increases. Overconsolidation can be caused by previous loading of the soil or desiccation. For a given soil, the tip stress increases with depth due to the increase in geostatic stresses.

TABLE 1 SUMMARY OF CPT SOUNDINGS ST-29 SITE PATRICK AFB, FL.

| Test ID | Date | Type | MW Type | Start Depth | Max Depth |
|----------------|-----------|---------|---------|-------------|-----------|
| CPT-86-01-LIF | 21-Mar-94 | CPT-LIF | | | 19.41 |
| CPT-86-01-MW | 21-Mar-94 | MW | Risers | | 8.3 |
| CPT-86-02-LIF | 21-Mar-94 | CPT-LIF | | | 16.06 |
| CPT-86-02-MW | 21-Mar-94 | MW | Tubing | | 8.14 |
| CPT-86-02-MW | 21-Mar-94 | MW | Risers | | 13.91 |
| CPT-86-02-SS01 | 24-Mar-94 | SS | | 3.5 | 4 |
| CPT-86-02-SS02 | 24-Mar-94 | SS | | 4 | 4.45 |
| CPT-86-02-SS03 | 24-Mar-94 | SS | | 4.45 | 5 |
| CPT-86-02-SS04 | 24-Mar-94 | SS | | 5.5 | 6 |
| CPT-86-02-SS05 | 24-Mar-94 | SS | | 6.2 | 6.8 |
| CPT-86-02-SS06 | 24-Mar-94 | SS | | 6.8 | 7 |
| CPT-86-03-LIF | 21-Mar-94 | CPT-LIF | | | 19.29 |
| CPT-86-03-MW01 | 21-Mar-94 | MW | Risers | | 19.54 |
| CPT-86-03-MW02 | 21-Mar-94 | MW | Tubing | | 14.08 |
| CPT-86-03-MW03 | 21-Mar-94 | MW | Risers | | 8.31 |
| CPT-86-03-SS01 | 24-Mar-94 | SS | | 3.33 | 3.92 |
| CPT-86-03-SS02 | 24-Mar-94 | SS | | 4.17 | 4.75 |
| CPT-86-03-SS03 | 24-Mar-94 | SS | | 4.83 | 5.33 |
| CPT-86-03-SS04 | 24-Mar-94 | SS | | 5.33 | 5.83 |
| CPT-86-04-LIF | 21-Mar-94 | CPT-LIF | | | 17.03 |
| CPT-86-04-MW | 21-Mar-94 | MW | Risers | | 10 |
| CPT-86-04-MW02 | 24-Mar-94 | MW | Riser | | 12.13 |
| CPT-86-05-LIF | 22-Mar-94 | CPT-LIF | | | 19.3 |
| CPT-86-05-MW01 | 22-Mar-94 | MW | Risers | | 20.02 |
| CPT-86-05-MW02 | 24-Mar-94 | MW | Riser | | 8.05 |
| CPT-86-05-A1 | 24-Mar-94 | SS | | | |
| CPT-86-05-A2 | 24-Mar-94 | SS | | | |
| CPT-86-05-A3 | 24-Mar-94 | SS | | | |
| CPT-86-05-A4 | 24-Mar-94 | SS | | | |
| CPT-86-05B-LIF | 22-Mar-94 | CPT-LIF | | | 19.73 |
| CPT-86-06-LIF | 22-Mar-94 | CPT-LIF | | | 16.09 |
| CPT-86-06-MW01 | 22-Mar-94 | MW | Riser | | 8.01 |
| CPT-86-07-LIF | 22-Mar-94 | CPT-LIF | | | 16 |
| CPT-86-07-MW01 | 22-Mar-94 | MW | Riser | | 8 |
| CPT-86-08-LIF | 22-Mar-94 | CPT-LIF | | | 19.51 |
| CPT-86-08-MW01 | 22-Mar-94 | MW | Tubing | | 8.01 |
| CPT-86-09-LIF | 22-Mar-94 | CPT-LIF | | | 19.35 |
| CPT-86-09-MW01 | 22-Mar-94 | MW | Risers | | 8.06 |
| CPT-86-09-MW01 | 24-Mar-94 | MW | Riser | | 8 |
| CPT-86-09-MW02 | 24-Mar-94 | MW | Tube | | 15 |
| CPT-86-09-A4 | 24-Mar-94 | SS | | 2.5 | 3.5 |
| CPT-86-09-A5 | 24-Mar-94 | SS | | 3.5 | 4.5 |
| CPT-08-09-A6 | 24-Mar-94 | SS | | 4.5 | 5.5 |

TABLE 1. SUMMARY OF CPT SOUNDINGS ST-29 SITE PATRICK AFB, FL.

(concluded)

| Test ID | Date | Type | MW Type | Start Depth | Max Depth |
|----------------|-----------|---------|---------|-------------|-----------|
| CPT-86-10-LIF | 22-Mar-94 | CPT-LIF | | | 19.48 |
| CPT-86-10-MW01 | 22-Mar-94 | MW | Risers | | 8 |
| CPT-86-11-LIF | 23-Mar-94 | CPT-LIF | | | 15.72 |
| CPT-86-11-MW01 | 23-Mar-94 | MW | Tube | | 8 |
| CPT-86-12-LIF | 23-Mar-94 | CPT-LIF | | | 15.99 |
| CPT-86-12-MW01 | 23-Mar-94 | MW | Tube | | 16.02 |
| CPT-86-12-MW01 | 24-Mar-94 | MW | Riser | | 8.07 |
| CPT-86-12B-LIF | 23-Mar-94 | CPT-LIF | | | 15.71 |
| CPT-86-13-LIF | 23-Mar-94 | CPT-LIF | | | 17.47 |
| CPT-86-13-MW01 | 23-Mar-94 | MW | Tube | | 17.49 |
| CPT-86-13-SS01 | 24-Mar-94 | SS | | 4.5 | 6.5 |
| CPT-86-14-LIF | 23-Mar-94 | CPT-LIF | | | 16.71 |
| CPT-86-14-MW01 | 23-Mar-94 | MW | Tube | | 16.73 |
| CPT-86-15-LIF | 23-Mar-94 | CPT-LIF | | | 19.39 |
| CPT-86-16-LIF | 23-Mar-94 | CPT-LIF | | | 19.5 |
| CPT-86-16-MW01 | 24-Mar-94 | MW | Riser | | 8.01 |
| CPT-86-16-MW03 | 24-Mar-94 | MW | Riser | | 45 |
| CPT-86-16-SS01 | 24-Mar-94 | SS | | 3 | 5.35 |
| CPT-86-16-SS02 | 24-Mar-94 | SS | | 5.35 | 7.7 |
| CPT-86-17-LIF | 23-Mar-94 | CPT-LIF | | | 14.6 |
| CPT-86-18-MW01 | 23-Mar-94 | MW | Riser | | 3.16 |
| CPT-86-18-MW01 | 23-Mar-94 | MW | Tube | | 16 |
| CPT-86-18-MW02 | 31-Mar-94 | MW | Riser | | 8 |
| CPT-86-18-MW03 | 31-Mar-94 | MW | Riser | | 40 |
| CPT-86-19-MW01 | 23-Mar-94 | MW | Tube | | 16 |
| CPT-86-19-MW02 | 23-Mar-94 | MW | Riser | | 8 |
| CPT-86-20-MW01 | 23-Mar-94 | MW | Tube | | 16.07 |
| CPT-86-20-MW02 | 23-Mar-94 | MW | Riser | | 8 |
| CPT-86-21-MW01 | 24-Mar-94 | MW | Riser | | 8 |
| CPT-86-21-MW02 | 24-Mar-94 | MW | Tube | | 15.3 |
| CPT-86-21-MW03 | 24-Mar-94 | MW | Riser | | 8.05 |
| CPT-86-22-LIF | 24-Mar-94 | CPT-LIF | | | 14.81 |
| CPT-86-22-MW01 | 24-Mar-94 | MW | Riser | | 13.46 |
| CPT-86-22-MW02 | 24-Mar-94 | MW | Riser | | 8.06 |
| CPT-86-23-MW01 | 25-Mar-94 | MW | Riser | | 7.01 |
| CPT-86-23-MW02 | 25-Mar-94 | MW | Riser | | 13.5 |
| CPT-86-24-MW01 | 25-Mar-94 | MW | Riser | | 6.5 |
| CPT-86-24-MW02 | 25-Mar-94 | MW | Riser | | 13 |
| CPT-86-25-MW01 | 25-Mar-94 | MW | Riser | | 6.5 |
| CPT-86-25-MW02 | 25-Mar-94 | MW | Riser | | 13 |
| CPT-86-26-MW01 | 25-Mar-94 | MW | Riser | | 7 |
| CPT-86-26-MW02 | 25-Mar-94 | MW | Riser | | 13.5 |

TABLE 2 SUMMARY OF CPT SOUNDINGS; FORMER FIRE TRAINING AREA, KENNEDY SPACE CENTER, CAPE CANAVERAL, FLORIDA

| Test ID | Date | Type | MW Type | Start Depth | Max Depth |
|------------------|-----------|---------|------------|----------------|--------------|
| CCAFB-01 | 29-Mar-94 | CPT-LIF | | | 14.31 |
| CCAFB-01-SS01 | 30-Mar-94 | SS | | 5.50 | 7.50 |
| CCAFB-01-SS02 | 30-Mar-94 | SS | | 7.50 | 9.50 |
| CCAFB-01B-SS01 | 30-Mar-94 | SS | | 5.50 | 7.50 |
| CCAFB-01B-SS02 | 30-Mar-94 | SS | | 7.50 | 9.50 |
| CCAFB-02 | 29-Mar-94 | CPT-LIF | 1 | | 10.12 |
| CCAFB-03 | 29-Mar-94 | CPT-LIF | | | 15.30 |
| CCAFB-04 | 29-Mar-94 | CPT-LIF | | | 13.23 |
| CCAFB-05 | 29-Mar-94 | CPT-LIF | | | 15.01 |
| CCAFB-06 | 29-Mar-94 | CPT-LIF | | | 15.81 |
| CCAFB-06-SS01 | 30-Mar-94 | SS | | 3.50 | 5.50 |
| CCAFB-06-SS02 | 30-Mar-94 | SS | | 5.50 | 7.50 |
| CCAFB-07 | 29-Mar-94 | CPT-LIF | | | 14.51 |
| CCAFB-07-SS01 | 30-Mar-94 | SS | | 5.50 | 7.50 |
| CCAFB-07-SS02 | 30-Mar-94 | SS | | 7.50 | 9.50 |
| CCAFB-08 | 29-Mar-94 | CPT-LIF | | | 15.03 |
| CCAFB-09 | 29-Mar-94 | CPT-LIF | | | 19.01 |
| CCAFB-10 | 29-Mar-94 | CPT-LIF | | | 18.74 |
| CCAFB-11 | 29-Mar-94 | CPT-LIF | | | 19.00 |
| CCFTA2-07-MW01M | 31-Mar-94 | MW | Tube | | 31.50 |
| CCFTA2-CPT-MW01D | 30-Mar-94 | MW | Riser | | 52.50 |
| CCFTA2-CPT-MW01M | 30-Mar-94 | MW | Riser | | 32.50 |
| CCFTA2-CPT-MW01S | 30-Mar-94 | MW | Riser | | 10.00 |
| CCFTA2-CPT-MW02S | 31-Mar-94 | MW | Riser | | 8.00 |
| CCFTA2-CPT-MW02M | 31-Mar-94 | MW | Tube | | 27.20 |
| CCFTA2-CPT-MW03D | 31-Mar-94 | MW | Tube | | 53.00 |
| CCFTA2-CPT-MW03M | 31-Mar-94 | MW | Tube | | 31.00 |
| CCFTA2-CPT-MW03S | 31-Mar-94 | MW | Riser | | 9.00 |
| CCFTA2-CPT-MW04M | 31-Mar-94 | MW | Tube | | 30.00 |
| CCFTA2-CPT-MW04S | 31-Mar-94 | MW | Riser | | 8.00 |

The friction ratio is a good indicator of the cohesiveness of the soil, which in turn reflects the fine-grained soil content. Soils that are predominantly fine grained have friction ratios generally greater than 2, and sandy soils have ratios of 2 or less. Weak and sensitive clays will have friction ratios of less than 2. The penetration pore pressure response is a function of the soil's shear strength and stiffness, hydraulic conductivity and density. For normally consolidated soils, the penetration pore pressure will be greater than the static pore pressure for clays and silts and equal to the static pore pressure for clean sands. In overconsolidated, dense soils the pore pressure response can be less than the static pore pressure, especially in those soils that tend to

dilate, such as silty sands. The combination of the friction ratio and pore pressure response provides a good identification of the soil lithology. With this basic understanding of the CPT data, an analyst can interpret the lithology and soil classifications visually as described below.

A typical penetration profile from Patrick AFB is presented in Figure 2. This profile (CPT-86-02-LIF) was completed to a depth of 15.4 feet below ground surface (bgs) and is representative of the geologic conditions at Patrick AFB. This profile includes the sleeve stress, tip resistance, friction ratio, penetration pore pressure, and baseline LIF counts measured during the test, along with the soil classification and soil lithology derived from the data. For location CPT-86-02-LIF, the friction ratio is fairly consistent throughout the profile. The classification profile derived from the friction ratio and pore-water pressure data indicates that the sediments consist of various gradations of sand. There are two zones at a depth of approximately 4 and 8.5 feet bgs that yield slightly higher friction ratios. These two zones represent transitions into finer grained soils. At approximately 9.5 feet bgs, the tip and sleeve stresses both increase somewhat linearly indicating zones of overconsolidated deposits.

B. INTERPRETATION OF LIF PROFILES

The LIF system accumulates data at a rate of approximately one (1) waveform per second, which correlates to one waveform every 2 centimeters as the LIF sensor is advanced into the formation. Each waveform consists of 125 data points, and when integrated yields the LIF-intensity value at a particular depth. The LIF data files showed a baseline-shift, apparently due to background noise from various sources. To compensate for this shift, the data sets were modified by subtracting out the average of the first five data points in each waveform before integration. This produces a waveform with a zero baseline. To compensate for instrument fluctuations, the LIF profile is further modified. The median of the lowest 41 LIF intensity values is subtracted from all LIF values in that profile. This number is called the time base for that profile. The data are subsequently plotted incorporating the above modifications.

The LIF profile for CPT-86-02-LIF shown in Figure 2 shows a significant LIF response at approximately 5 feet bgs. This correlates well with the estimated depth of the water table located at 5.5 feet bgs. This suggests that the LNAPL contamination lies at or slightly above the water table at this location. This profile is included in Appendix A along with the profiles from all of the soundings completed at both Patrick AFB and Kennedy Space Center.

Figure 2. LIF-CPT profiles for CPT-86-02-LIF.

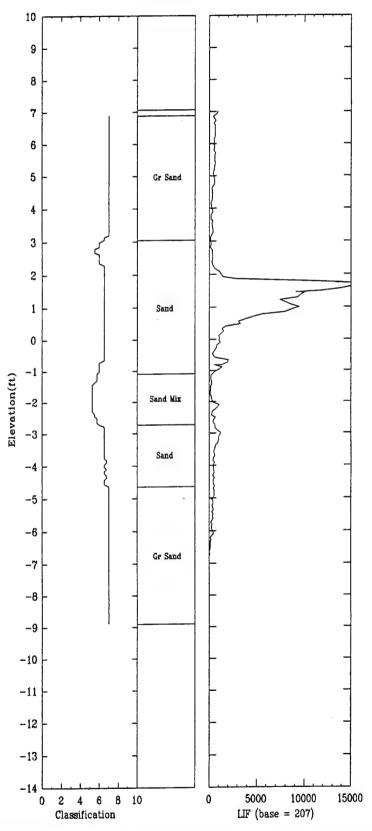


Figure 2a.LIF-CPT profiles for CPT-86-02-LIF (concluded).

Analysis of the LIF-CPT profiles contained in Appendix A was completed to define both the horizontal and vertical extent of the contamination plume. Locations CPT-86-02-LIF, CPT-86-03-LIF, CPT-86-09-LIF and CPT-86-10-LIF all recorded large LIF values indicating significant levels of contamination. These locations are centered just west of the grassy area between the Base Service Station and the tarmac. Other neighboring locations such as CPT-86-06-LIF, CPT-86-08-LIF, CPT-86-07-LIF and CPT-86-16-LIF all exhibit smeared contamination with LIF values above baselines for much of the penetration profile. Based upon this analysis, an LIF detection level plume has been located on Figure 1. Analysis similar to this was used directly in the field to guide investigation and site many of the monitoring wells.

SECTION IV CONCLUSIONS

The CPT-LIF proved a useful and efficient tool for conducting subsurface site investigations at both the SS-29 site located at Patrick AFB in Cocoa Beach, FL and the former fire training facility located at the Kennedy Space Center, Cape Canaveral, FL. The CPT data accurately described the lithology of the SS-29 site as various gradations of sands with occasional discontinuous seams of silty clays and clay. This interpretation closely matches interpretations described by others during previous investigations. The CPT data were used to effectively set monitoring wells and collect soil samples. The LIF data assisted in defining both the horizontal and vertical extent of the liquid phase plume. A complete report assessing all the data collected during the course of this investigation including the groundwater and soil chemical analytical data are contained in Volume I of this report.

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- 1. Engineering-Science, Inc. (ES), "Draft Work Plan for an Engineering Evaluation/Cost Analysis in Support of the Intrinsic Remediation (Natural Attenuation) Option," for Patrick AFB, Florida, ES, Denver, Colorado, March 1994.
- 2. Environmental Science and Engineering, Inc. (ESE), "Installation Restoration Program, Air Force Installation Restoration Program, Phase II, Stage 2, Remedial Investigation/Feasibility Study, for Patrick Air Force Base, Cocoa Beach, Florida," Vol. I through Vol X, Gainesville, Florida, 1991.
- 3. O'Brien and Gere Engineers, Inc., "ST-29 (PPOL-2) Work Plan Draft Final Report," Patrick AFB, Florida.
- Environmental Science and Engineering, Inc. (ESE), "Installation Restoration Program, Phase I: Records Search, Eastern Space and Missile Center: Patrick Air Force Base, Florida,"
 Gainesville, Florida, 1984.
- 5. Environmental Science & Engineering, Inc. (ESE), "Installation Restoration Program, Phase II: Confirmation/Quantification, Stage I, Patrick Air Force Base, Florida," Vol. I and Vol. II, 1988.
- 6. Engineering-Science, Inc. (ES), "Bioventing Test Work Plan and Interim Results Report for Three Bioventing Sites, Patrick Air Force Base and Cape Canaveral Air Force Station, Florida," Prepared for the Air Force Center for Environmental Excellence and 45CES/DEEV, Patrick Air Force Base, Florida, ES, Orlando, Florida, June, 1993.

APPENDIX A

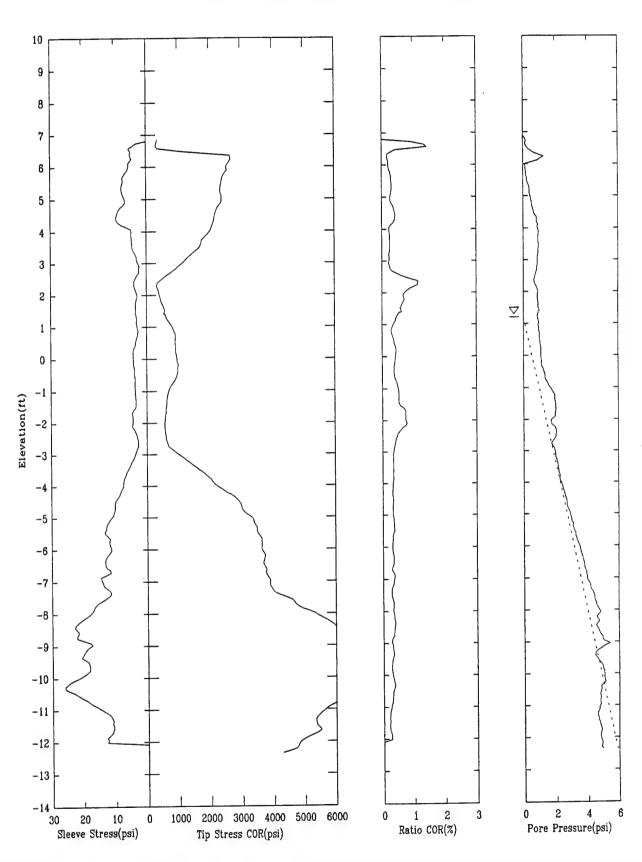
LIF-CPT SOUNDING PROFILES

03/21/94

North 491

East 363

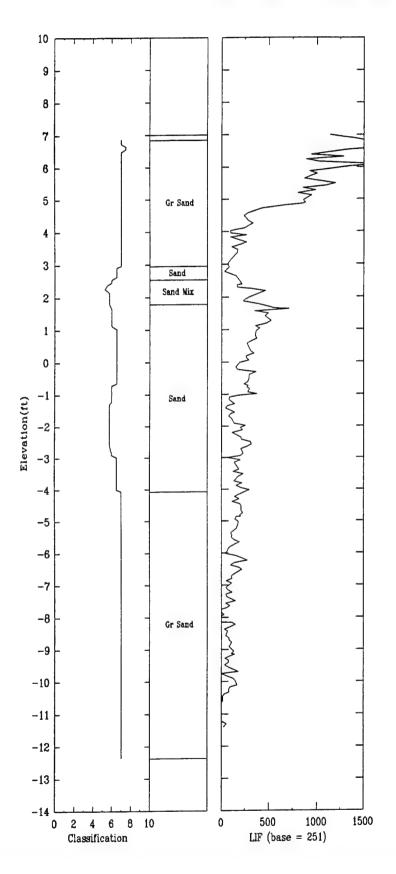
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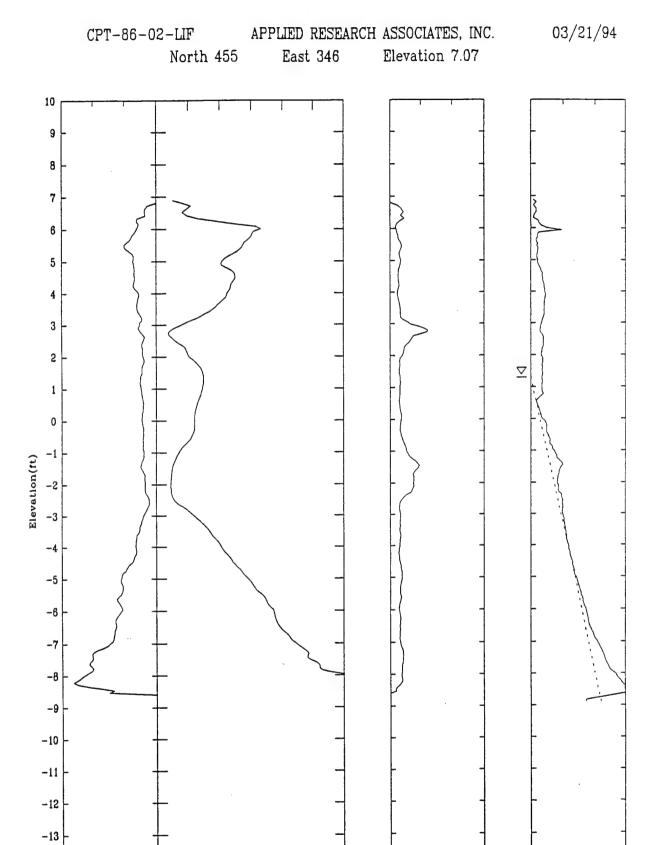


North 491

East 363

Elevation 7.02





1000 2000 3000 4000 5000 6000

Tip Stress COR(psi)

1 2 Ratio COR(%) 0 2 4 Pore Pressure(psi)

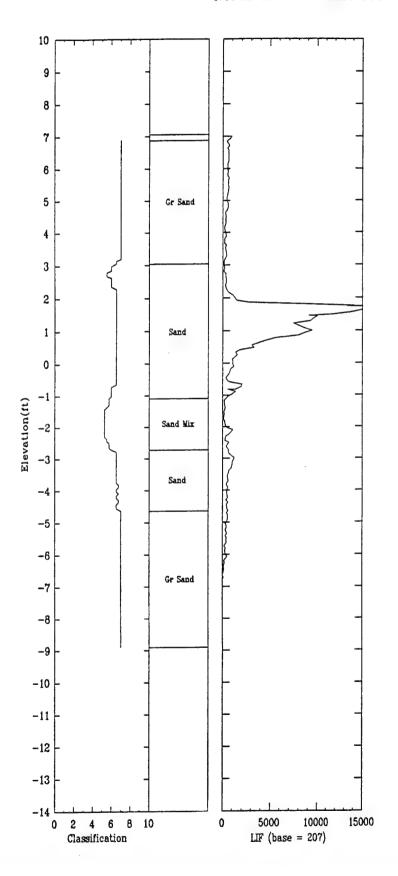
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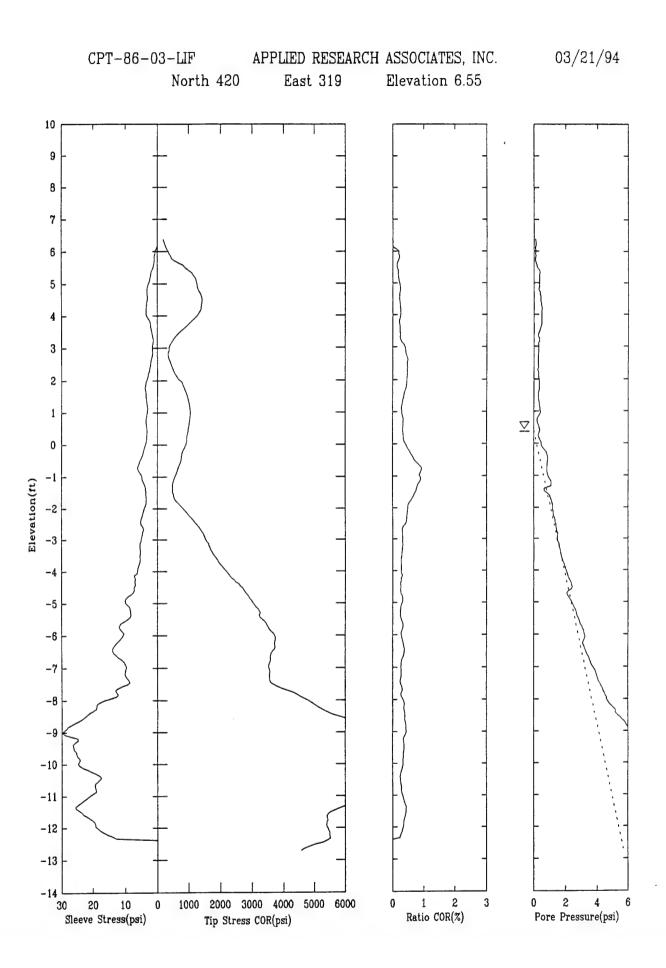
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0 20 10 Sleeve Stress(psi) North 455

East 346

Elevation 7.07

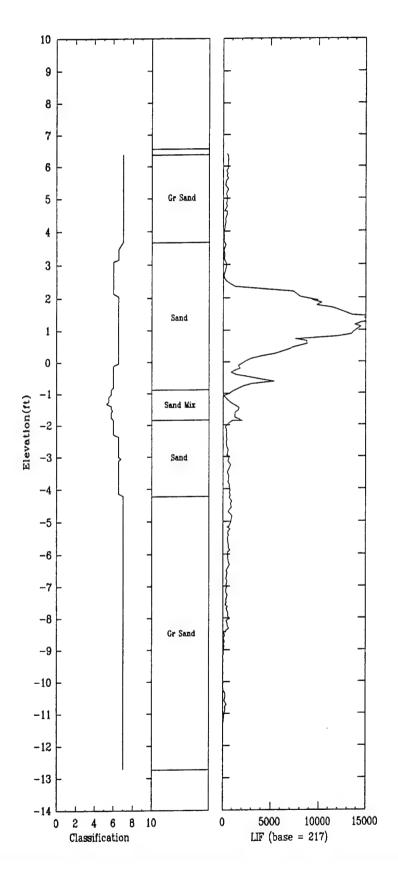




North 420

East 319

Elevation 6.55



2

Pore Pressure(psi)

Ratio COR(%)

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Tip Stress COR(psi)

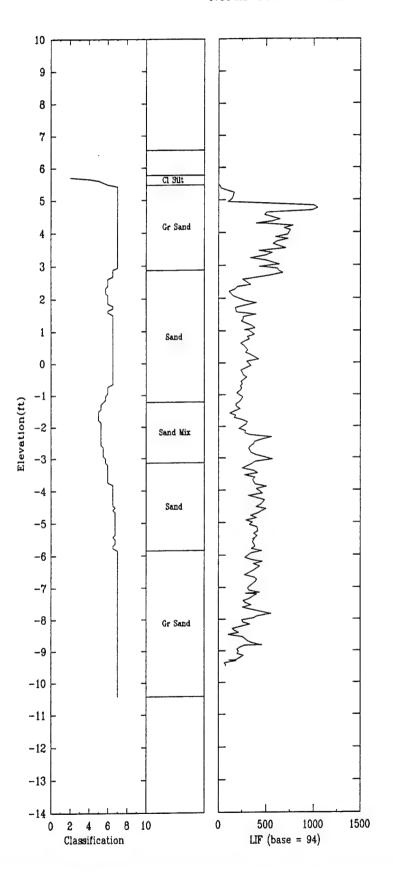
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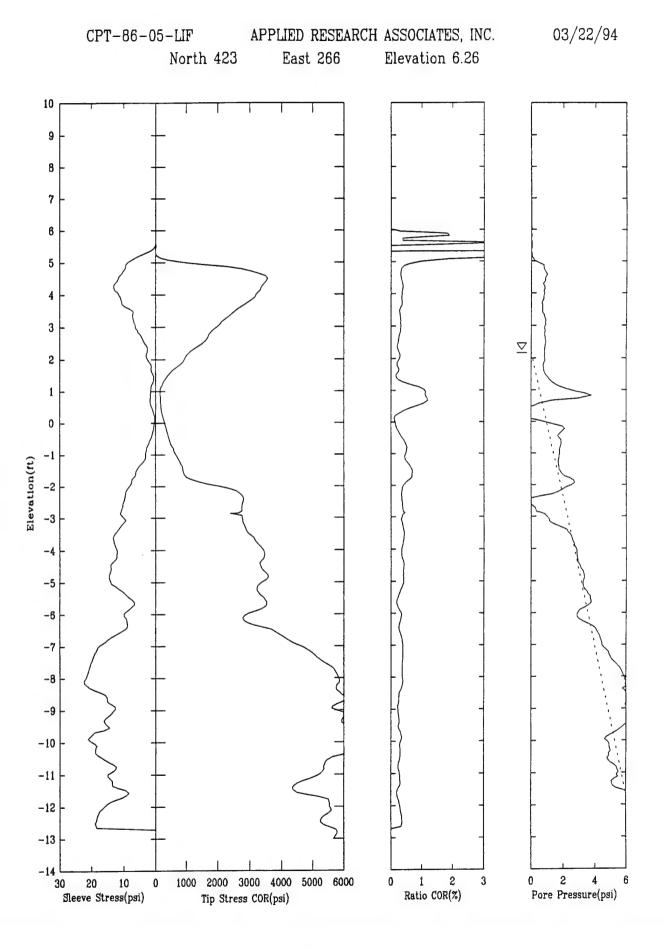
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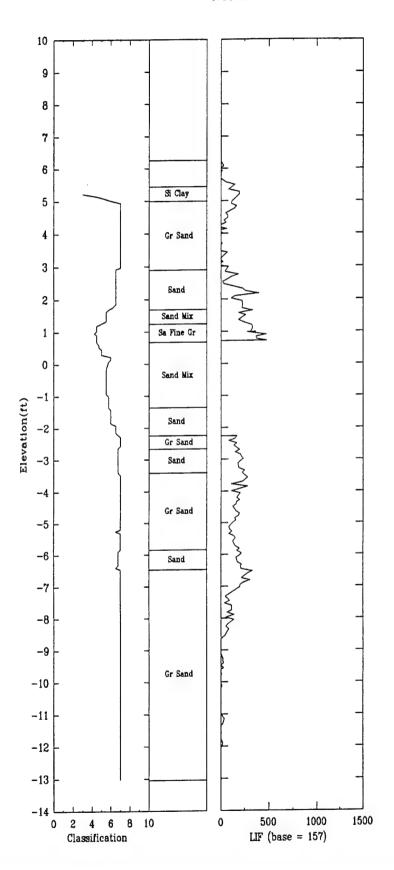
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East 133

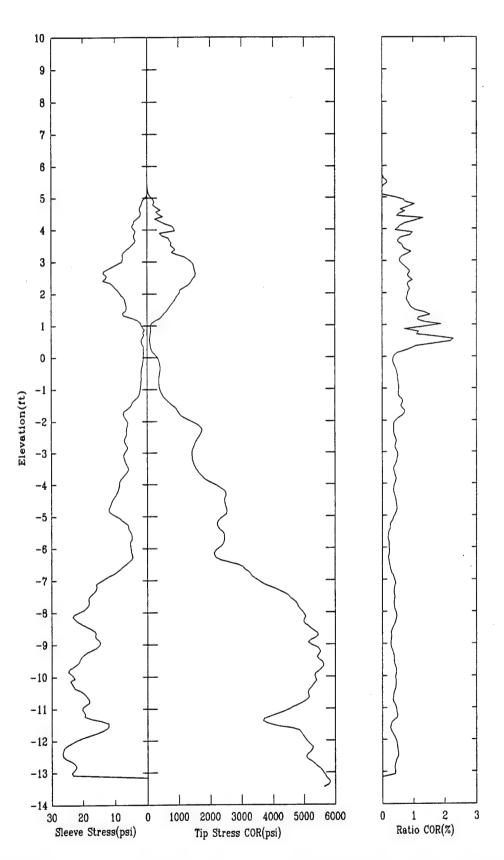




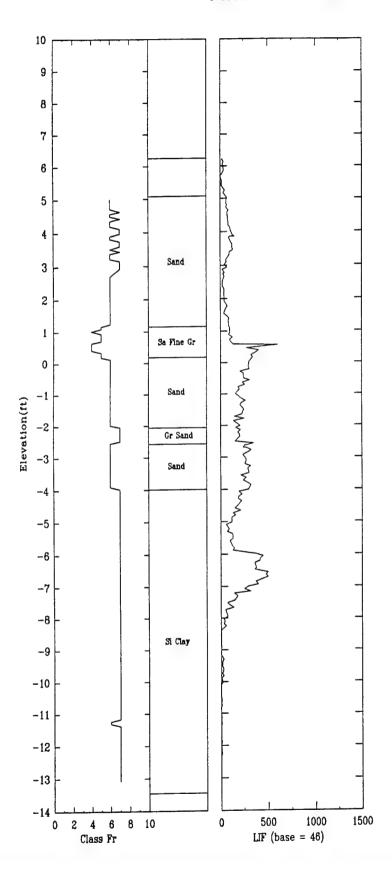
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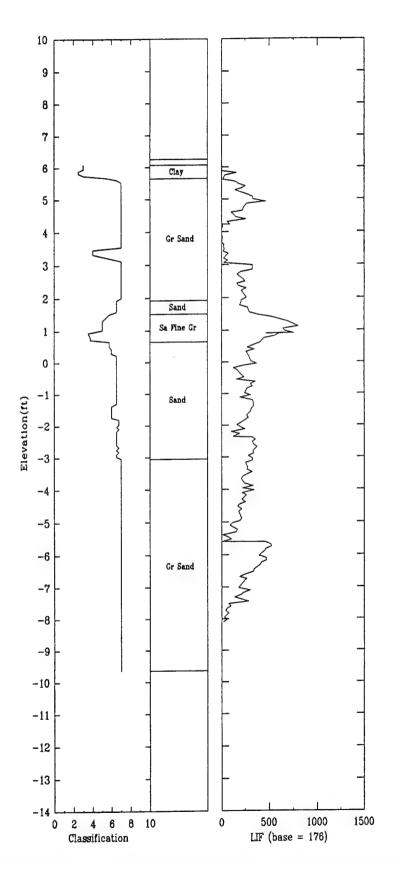
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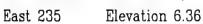
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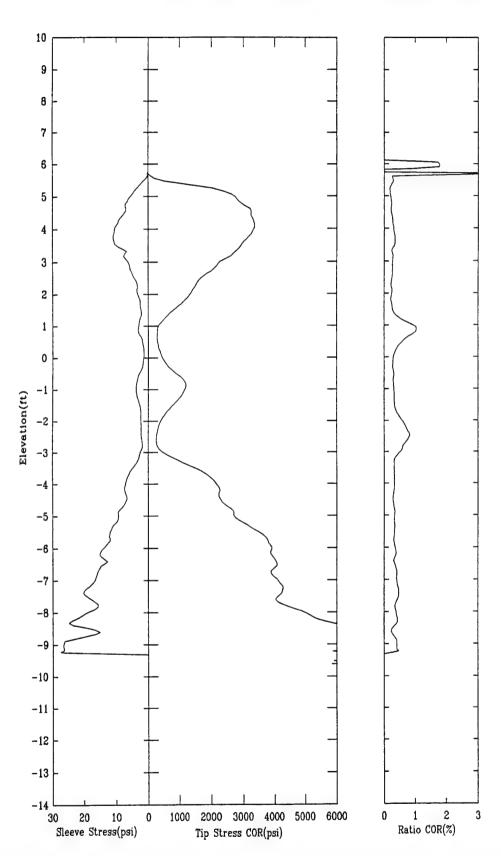


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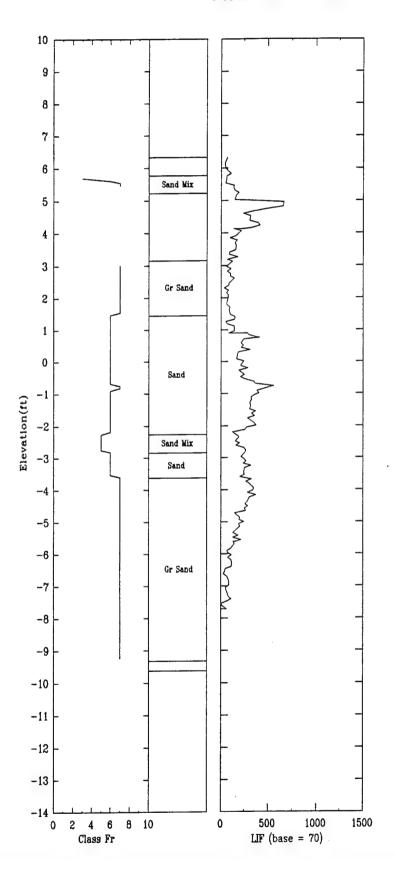


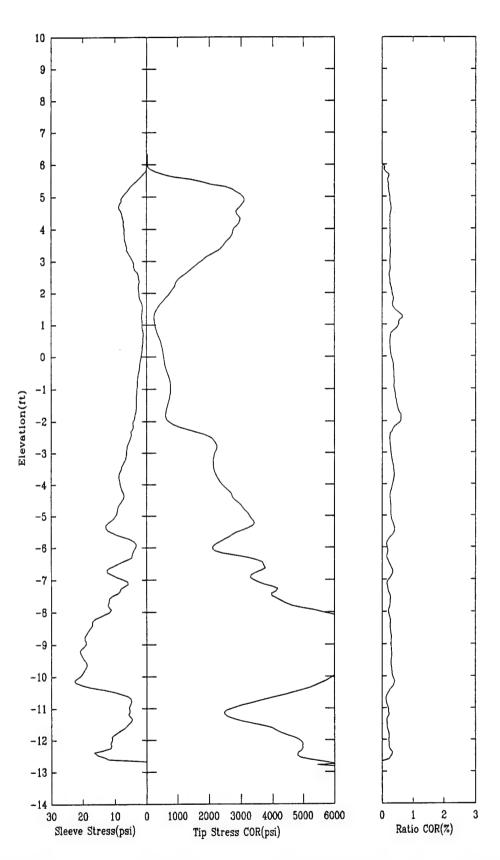




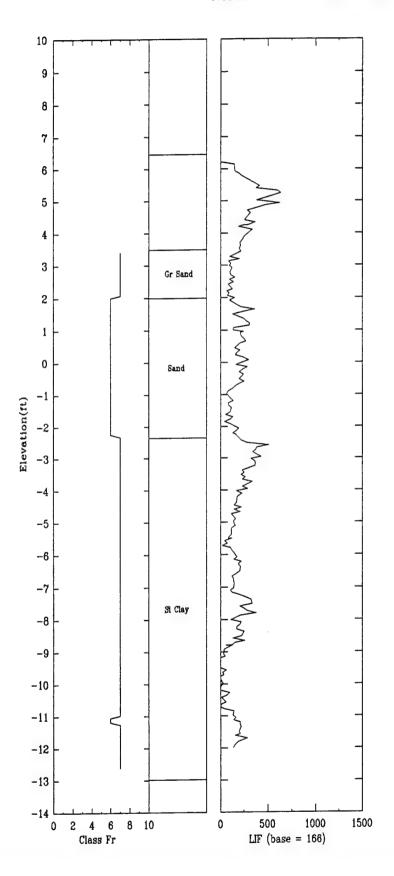


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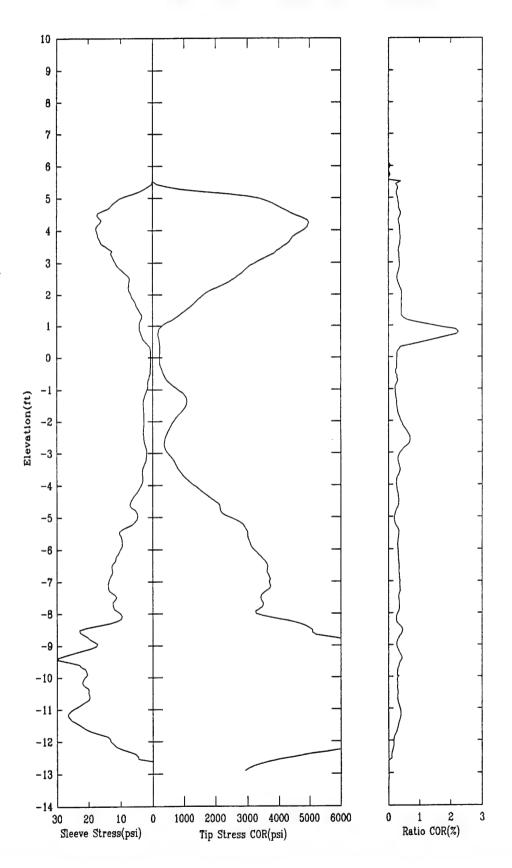




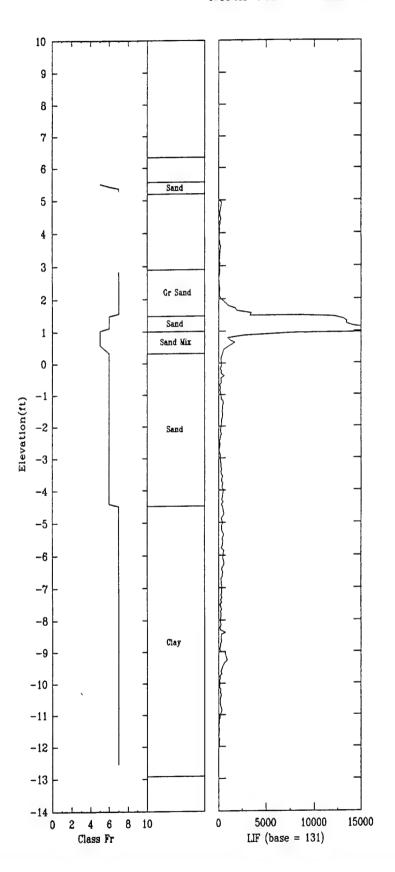
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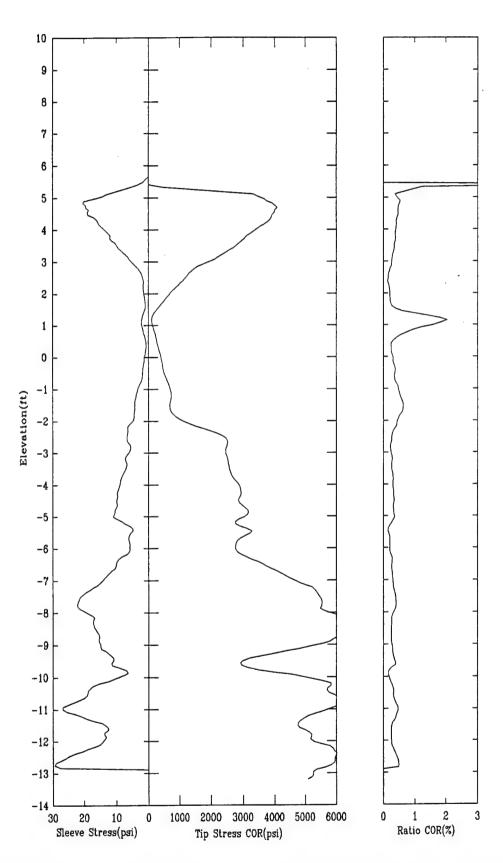
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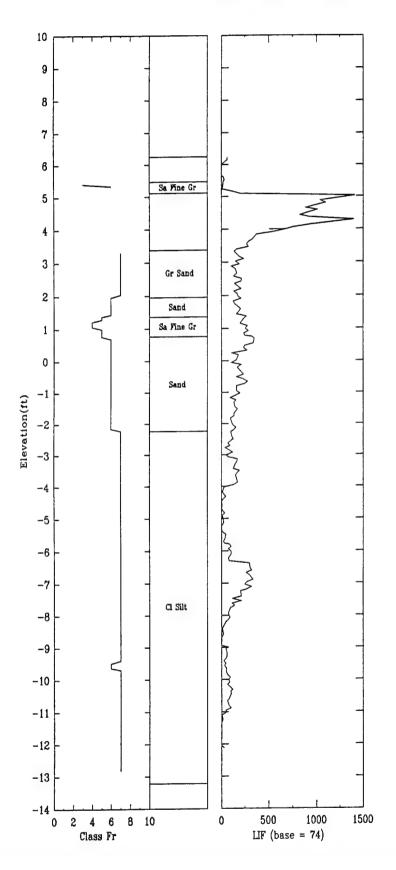


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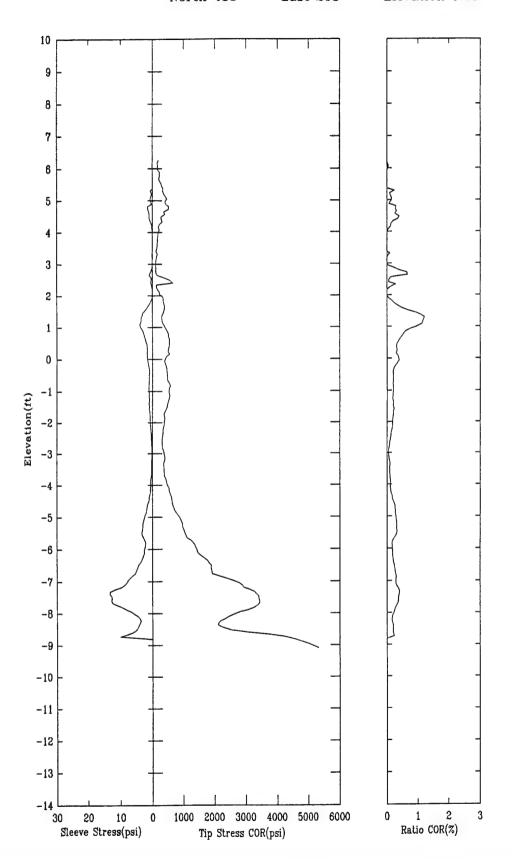


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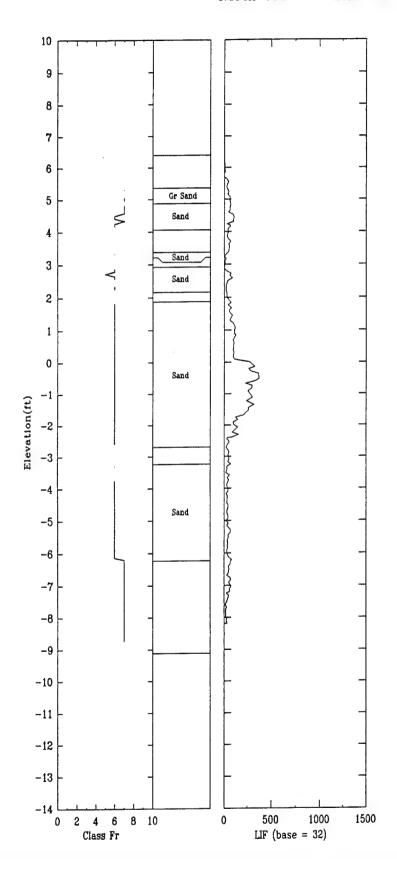


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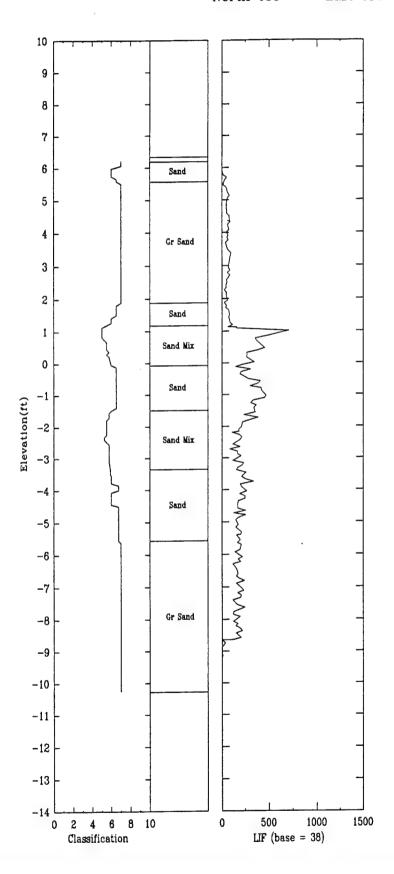
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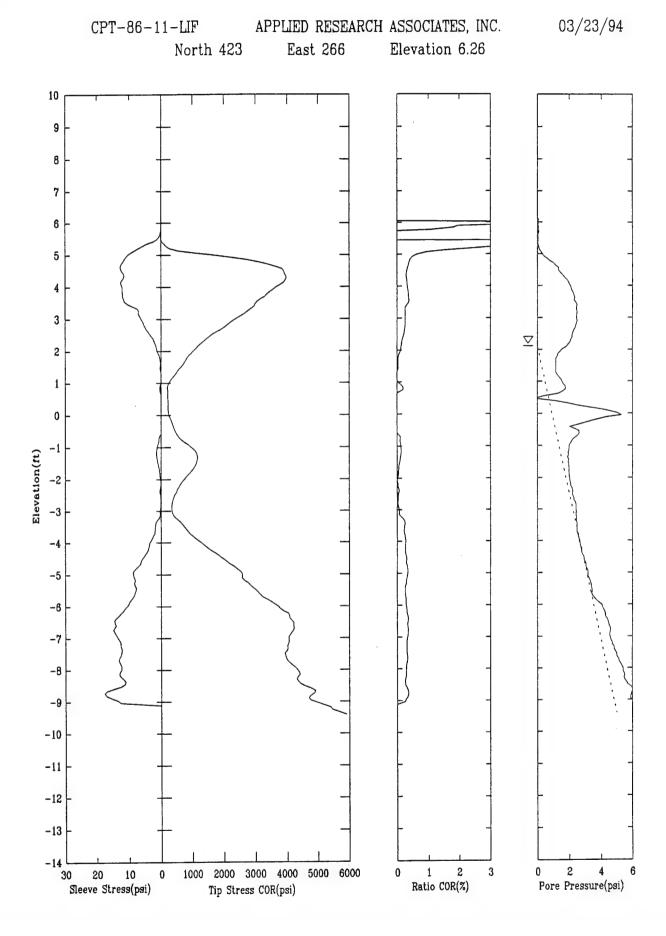
Elevation 6.43



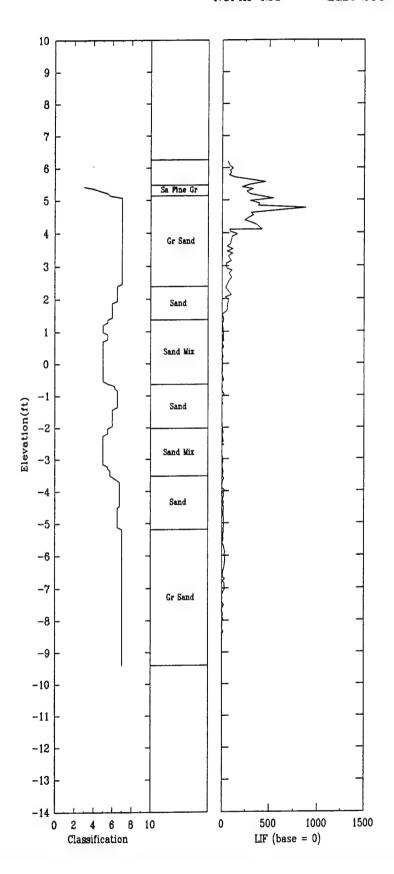
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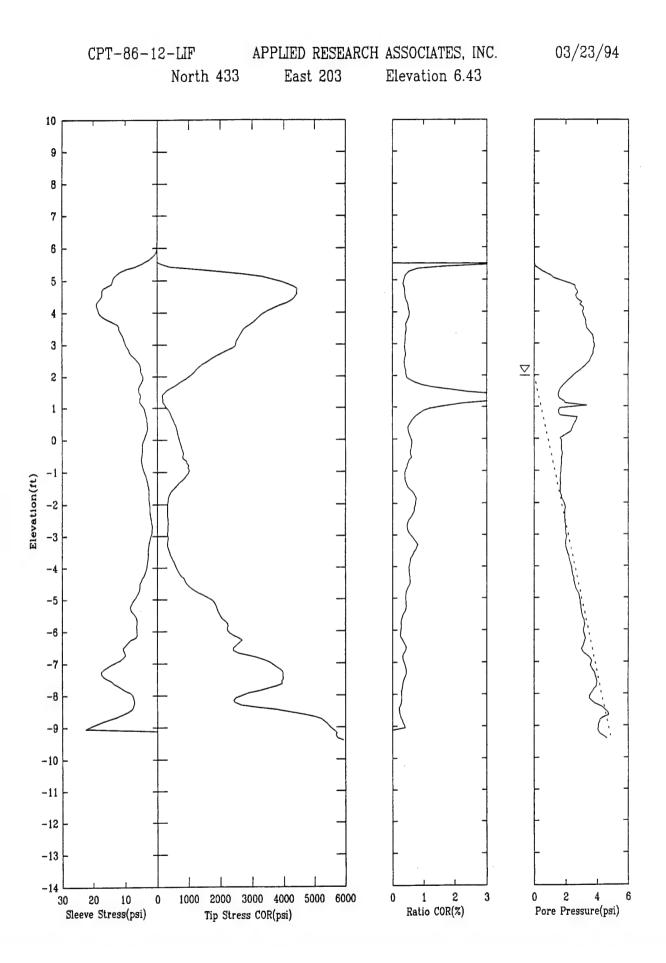
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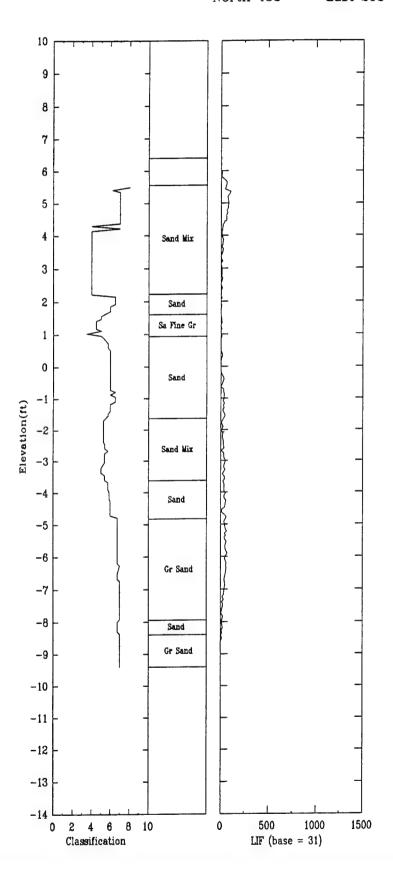


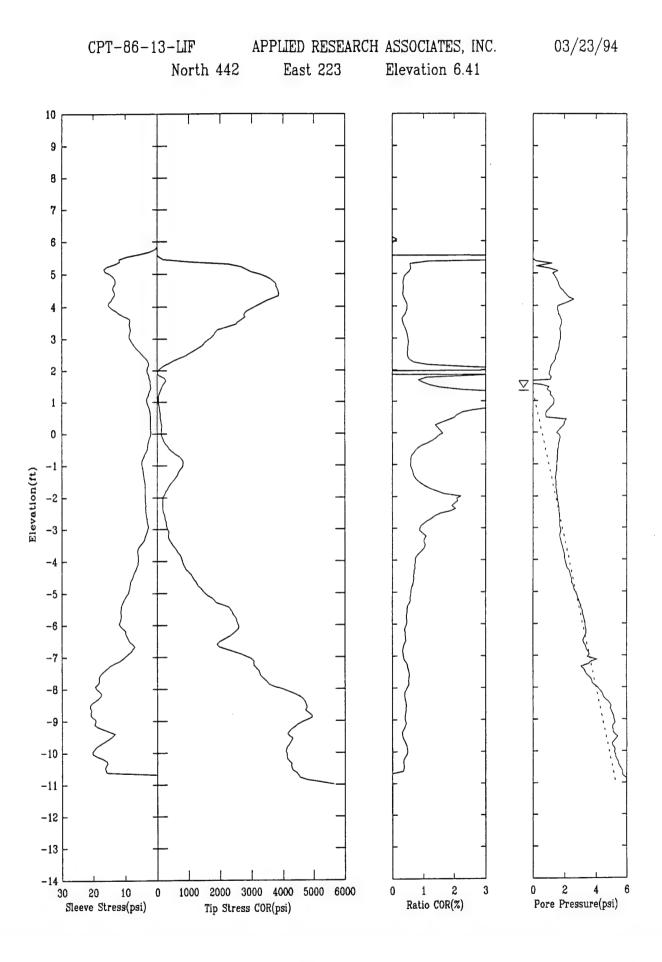
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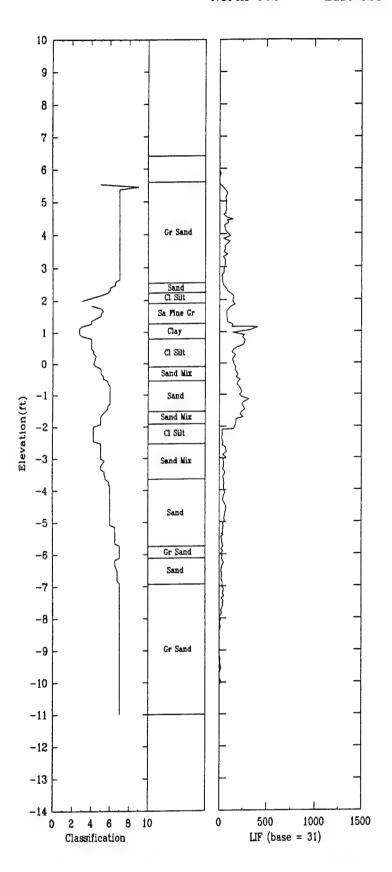


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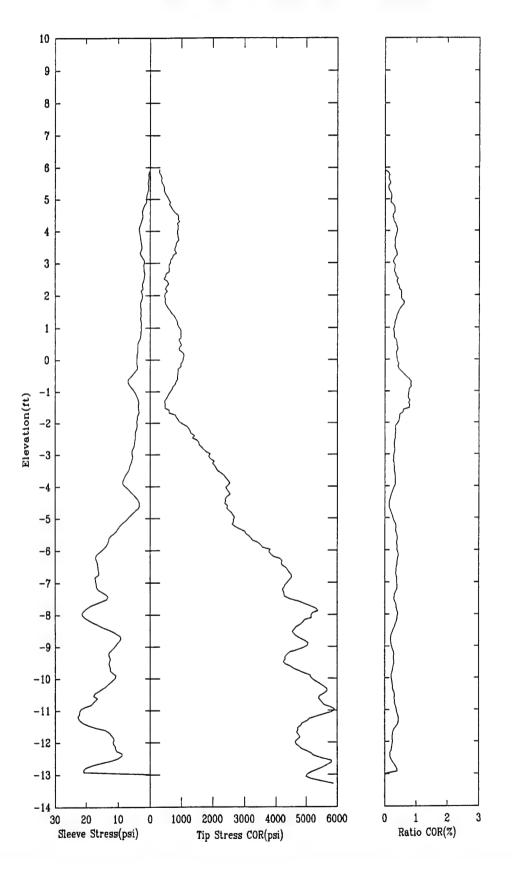




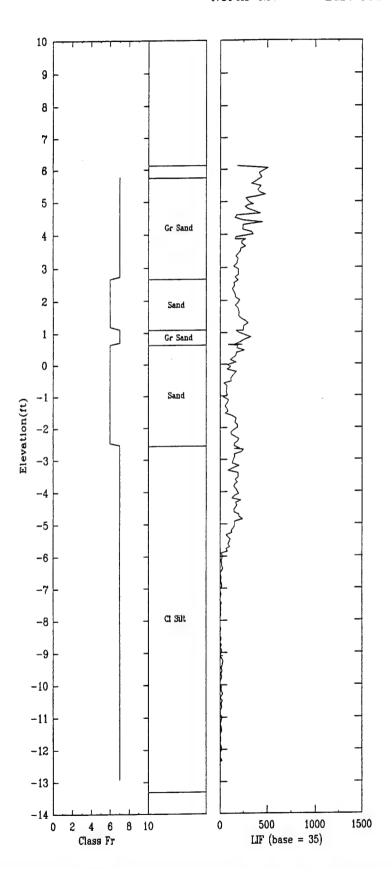
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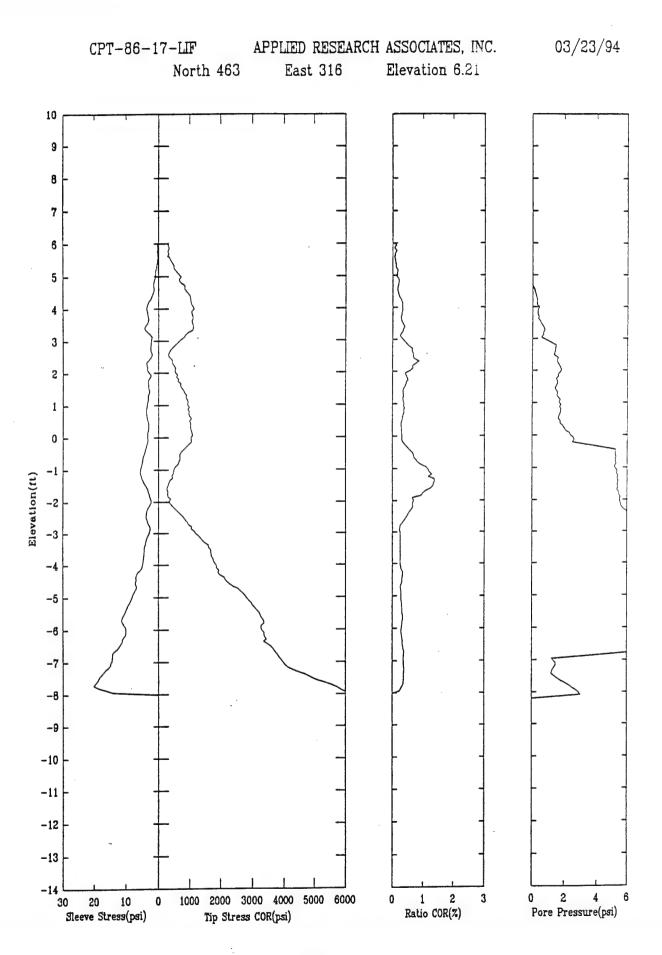


East 300



East 300





East 316

